## UNITED STATES PATENT APPLICATION

of

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for

# SIGNAL DERIVED BIAS SUPPLY FOR ELECTROSTATIC LOUDSPEAKERS

# TO THE COMMISSIONER OF PATENTS AND TRADEMARKS:

Your petitioners, Jeevan G. Bank and James J. Croft III, who are citizens of the United States, and whose residence and post office addresses are 8034 Camino Tranquilo, San Diego, California 92122 and 13633 Quiet Hills Drive, Poway, California 92604, respectively, pray that letters patent may be granted to them as the inventors of the improvement in a SIGNAL DERIVED BIAS SUPPLY FOR ELECTROSTATIC LOUDSPEAKERS, as set forth in the following specification.

#### TECHNICAL FIELD

This invention relates generally to the field of electrostatic speakers and more specifically to power supplies for biasing electrostatic speakers.

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#### **BACKGROUND ART**

The long history of electrostatic speakers has produced a wide variety of speaker configurations. To provide a linear output, an electrostatic speaker requires a high (500 to 5000 volts) substantially DC (direct current) voltage to be applied either to the stators or the diaphragm. This applied voltage creates a DC constant for the AC (alternating current) signal voltages to work against. Since only the leakage currents need to be supplied, the wattage rating of the fixed bias supply can be quite low (less than a watt) and the package size can be small (a few cubic inches).

Historically, this DC voltage has been provided by running a step-up transformer from an AC power line, rectifying its output, and connecting the rectified output to a capacitor. US patent 2,896,025 granted to Janszen embodies this approach. This configuration is easy to implement but can be somewhat costly. It can also be inconvenient to have to run separate AC main wires and also signal wires from the power amplifier. Additionally, if the AC power is intended to be supplied directly from a wall source, there may be no AC power sockets located nearby the electrostatic loudspeakers. Another drawback of using a separate AC power supply is that the separate power supply results in additional cost and wiring which makes electrostatic speakers a less desirable choice in most consumer applications. Thus, the electrostatic speakers

THORPE, NORTH & WESTERN, LLP P O Box 1219 Sandy, Utah 8491-1219 Telephone (801) 566-6633 Docket No. T8320 Rev 10/21/99 are less desirable even though they offer superior performance and greater sound fidelity when

they couple into the air.

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In particular applications where the systems run off of DC, such as a laptop computer or a

portable music system, a high voltage source of AC may not be available. In these applications,

a DC to DC converter is required to produce the required high voltages. This DC to DC

convertor system is illustrated in US patent 3,992,585 granted to Turner, et al.

Another method to provide a DC bias, which avoids many of the issues in the prior art

listed above, is to tap off of the secondary winding of the audio signal transformer. The tapped

voltage is then rectified and the energy is stored in a capacitor. Because the bias currents are

near zero, this approach has virtually no impact on the signal currents. Disclosures of this

technique can be found in US patent 3,895,193 granted to Bobb, US patent 4,160,882 granted to

Driver and US patent 5,392,358 granted to Driver.

For most consumer applications, what would be most useful, is a "drop in" replacement

for existing electromagnetic speakers. In other words, an electrostatic speaker which can

effectively replace existing electromagnetic speaker systems is desirable. This would eliminate

the need for an AC outlet or a DC to DC convertor and maintain a simple connection with two

wires for each speaker. Self-biasing can provide this, but the prior art systems all suffer from a

common group of significant drawbacks.

First, because the AC audio signal is not predictable or repeatable, the voltage available at

the output of the audio signal step-up transformer can vary from a zero voltage to a voltage that

can damage the electrostatic unit due to over voltage.

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A second problem with the prior art type of bias system is that when the audio equipment

is first powered up, the self-bias voltage (and hence the resulting electric field) is at, or close to

zero. As a result, there is a start up time during which the audio level gradually increases to the

maximum. During the charging period, the program signal will not be heard at its proper

volume. For certain types of music and some audio material, many seconds elapse before the

self-bias voltage comes into its normal range. One approach is to have a fast signal rise time

when the system is turned on. To increase the signal rise time, the transformer step-up ratio can

be increased but this can then make the first problem of over-voltage even worse.

A third problem is that prior art self-bias circuits provide a variable bias voltage. The

side effect of the variable bias voltage can best be described as producing a noticeable "pumping

action" in the reproduced acoustic output level.

A fourth problem with this type of bias system is that in a multi-channel system, each

channel can end up with different bias levels at any given time. Therefore, each channel would

have a different efficiency and would be mismatched depending on how well the multi-channel

program material was matched from channel to channel at any given moment.

**OBJECTS AND SUMMARY OF THE INVENTION** 

It is an object of the present invention to provide a bias system which uses a simple two

wire speaker connection and the reduces cost of self-biasing for DC field generation in the

electrostatic speaker.

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It is also an object to provide a bias system which uses an audio signal derived bias system for an electrostatic loudspeaker that steps up the voltage to the required level even with

program material at a low level, and maintains a substantially constant supply voltage.

It is another object of the current invention to provide a self bias system which uses a voltage limiting/regulating means in an output signal fed bias supply so the voltage is stabilized

to be substantially constant and limited from over voltage.

It is a further object of the invention to achieve a more effective startup than prior art

systems using the greater step-up ratio of the transformer secondaries.

It is an additional object of the invention to provide a more effective startup using greater

multiplication stages in the voltage multiplier circuit and a separate charging signal delivered

from the associated active electronics which charges on startup, periodically, or on a steady basis.

The presently preferred embodiment of the present invention is an audio signal derived

bias supply for use with an electrostatic loudspeaker. The bias supply includes at least one

transformer adapted to receive an audio signal. The transformer has at least one primary

winding, and primary connection taps. The transformer also has at least one secondary winding

magnetically coupled to the primary winding, which has at least two secondary connection taps.

A bias circuit is connected to the at least one secondary winding. The bias circuit has a

rectification means and a voltage limiting means, coupled to the rectification means.

These and other objects, features, advantages and alternative aspects of the present

invention will become apparent to those skilled in the art from a consideration of the following

detailed description taken in combination with the accompanying drawings.

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### **BRIEF DESCRIPTION OF THE DRAWINGS**

FIG. 1 shows a prior art self bias circuit:

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- FIG. 2 shows a block diagram of the signal derived bias supply;
- FIG. 3 shows a simple schematic diagram of the signal derived bias supply;
- FIG. 4A shows a simple schematic diagram of another form of the self bias supply;
- FIG. 4B shows a schematic diagram of a self bias supply using a voltage divider;
- FIG. 5 shows a form of the self bias supply using a transformer with more windings;
- FIG. 6 shows a schematic diagram of one implementation of a signal derived, self bias power supply;
  - FIG. 7 shows a block diagram of the signal derived self bias supply connected to a parametric loudspeaker;
  - FIG. 8 shows a schematic diagram of a signal derived self bias supply with two transformers connected to two electrostatic speakers;
  - FIG. 9 shows a schematic of a self bias supply where the zener diodes are located near the secondary winding taps;
  - FIG. 10 shows a self bias supply with the bias connected to a single stator and the signal connected to two separate diaphragms; and
- FIG. 11 shows a bias supply with one tap from the high voltage secondary winding coupled to the diaphragm, the bias return tap connected to the diaphragm, and one tap from the high voltage winding connected to the stator.

THORPE, NORTH & WESTERN, LLP P O Box 1219 Sandy, Utah 3491-1219 Telephone (801) 566-6633 Docket No T3320 Rev 10/21/99 **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS** 

Reference will now be made to the drawings in which the various elements of the present

invention will be given numerical designations and in which the invention will be discussed so as

to enable one skilled in the art to make and use the invention. It is to be understood that the

following description is only exemplary of certain embodiments of the present invention, and

should not be viewed as narrowing the claims which follow.

FIG. 1 represents a prior art self bias circuit for an electrostatic speaker. The transformer

10 accepts an input signal to a primary winding 12, which is then converted into a higher voltage

and output through the secondary winding 11. Lower voltage outputs 11c and 11d send audio

signals to stators 2a and 2b. Higher voltage taps 11a and 11b feed the voltage doubler 13, which

consists of diodes 13c and 13d, and capacitors 15a and 15b. The unregulated, non-limited

voltage signal is sent through resistor 17 to diaphragm 30. With this type of system, the voltage

varies up and down due to the dynamics of the program material and provides a substantially

alternating voltage to the diaphragm 30 instead of the preferred constant DC voltage. In

addition, there is no limit to the voltage buildup at the speaker diaphragm 30.

FIG. 2 shows a basic block diagram of the present invention. A program signal is

received by the transformer 10, and output to a voltage multiplier and rectifier means 13. The

voltage multiplier and rectification means 13 has a bias supply output 3a which is regulated and

limited by the voltage limiter 40. The output voltage 3a is then supplied to the electrostatic

diaphragm 30.

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FIG. 3 shows a schematic of a signal derived bias power supply in its most basic operational form. A program signal is received by the primary winding 12 of a transformer 10 and output as a higher voltage from the secondary winding 11 through the tap 51. The signal is rectified by a diode 13a and resistively coupled through a resistor 16 to a speaker diaphragm 30 and returns to the transformer center tap 50 through a voltage limiter 40 or shunt regulator which consists of a capacitor 41 and a zener diode 42. The conventional definition of a center tap is that an approximately equal number of secondary windings are on either side of the tap. It is important to realize that this invention will work with a center tap which does not have an equal number of secondary windings on either side of the center tap. Offsetting the center tap does mean that one side of the circuit produces a higher voltage than the other which is not necessarily desirable, but it is a workable configuration. In addition, the center tap could also be a bias return with another configuration such as a voltage divider or a similar arrangement.

Accordingly, as used in this application, center tap refers to a biasing tap separate from the stator taps 51.

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The zener diode 42 and capacitor 41 coupled to the secondary winding in the circuit shown in FIG. 3 perform a voltage regulation function. It should be realized based on this disclosure, that other voltage limiting means could be used in place of the zener diode and capacitor to perform a regulation function and protect the electrostatic diaphragm from over voltage. For example, a controlled spark gap component, transistors, or similar equivalent devices could be used for voltage regulation, although they might require other active circuitry to perform the regulation function.

FIG. 4A is essentially the same as FIG. 3 with an additional diode rectifier 13b to allow for a symmetrical contribution from both of the secondary taps 51 and 52 of the secondary

winding 11. Another important element that has been added is a resistor 17 to provide lower

distortion, and constant charge operation of the speaker diaphragm 30.

FIG. 4B shows a schematic diagram of a self bias supply using a voltage divider. The

arrangement of the rectifier diodes 13a and 13b and the bias circuit with the zener diode(s) 42

and capacitor 41 are the same as in FIG. 4A. An important part of FIG. 4B is that the center tap

or bias return in FIG. 4A has been synthesized using a voltage divider which is connected to the

transformer 10. The primary signal 12 which enters the transformer 10 is stepped up through the

secondary windings 11. Then instead of a center tap, the two resistors 46 reduce the voltage at

the connection 44 to a lower voltage similar to one that would be received from a center tap.

FIG. 5 is an alternative embodiment of the functionality shown in FIG. 4A. The voltage

bias supply in FIG. 5 is fed off of the high voltage secondary taps 53 and 54. Adding the

resistors 14a and 14b further isolates the voltage limiter 40 from any discontinuities produced by

fluctuations in the secondary winding taps 51 and 52. Although a single secondary winding with

multiple taps is shown, it should be apparent based on this disclosure that many separate

secondary windings could be provided and wrapped around the same transformer core. In FIG.

5, a separate winding could be used for each voltage which is desired. For example, a separate

high voltage winding could be used between taps 53 and 54, and then a separate lower voltage

winding could be used between taps 51 and 52. Other alternative winding arrangements could

also be conceived.

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FIG. 6 represents a preferred embodiment of the invention and describes a more complex

embodiment that is used to implement the simpler forms of the other figures. Referring now to

FIG. 6, the audio signal from a power amplifier is first applied to the input 12 of a step-up or

matching transformer 10. The secondary winding 11 of the transformer 10 provides a high

voltage and high impedance output, which drives the stators of the electrostatic speaker.

Additionally, the secondary winding 11 of the transformer 10 has a center-tap connection 50.

The details of the circuit operation in FIG. 6 will now be described. The high voltage

output of the transformer 10 drives the stators through the resistors 1a and 1b which provide high

frequency equalization of the audio output. Additionally, the high voltage outputs of the

transformer are applied to the voltage multiplier/rectifier circuit 13, consisting of diodes 13c and

13d, resistors 14a, 14b, 14c, 14d, capacitors 15a and 15b, followed by resistors 16a, 16b, 16c,

16d. The resistors (14a, 14b, 14c, 14d, 16a, 16b, 16c, 16d) limit the maximum loading on the

transformer 10 during surges in the audio output level, which avoids any noticeable distortion of

the output signal to the stators 2a, 2b. Capacitors 15a and 15b and the high voltage diodes 13c

and 13d form a conventional voltage doubling circuit and provide a rapid build up of DC voltage

on the diaphragm 3 with respect to the stators.

The DC voltage is applied through the diode 13d, and resistors 16a through 16d (in

series) to a group of zener diodes 42a which are in series. These resistors and diodes clamp the

DC level at the desired bias voltage and prevent any variation in the DC field as the level of the

audio source fluctuates. For example, each of the 10 zener diodes would have a 200 volt rating

which provides clamping at 2000 volts.

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The capacitor 41 is also charged while biasing zener diodes 42a into their zener region.

Although resistors 16a-16c are large enough to prevent any noticeable distortion of the audio, the

combined R-C time constant is low enough to add only a negligible amount of delay to the

charge time of capacitor 41. Resistors 17a and 17b provide a high degree of isolation (on the

order of 10s of megohms) between the self-generated high voltage and the diaphragm so that the

diaphragm operates in a "constant charge" mode and only a very small current flow

(microamperes) can occur between the diaphragm 30 and the stators 2a and 2b with their highly

variable voltages.

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In addition to what has been described, diode 13e provides reverse isolation so that the

capacitor 41, across the fully biased zener diode string 42a, will not be drained during periods

when the average voltage level falls and the rectified output presented to diode 13e is less than

the voltage across capacitor 41.

The polarities used in the examples above have been arbitrarily chosen to produce a

negative voltage on the diaphragm with respect to the stators. To change this to a positive

voltage all of the diodes would be turned around.

In several cases, there are multiple resistors placed in series where it would seem that a

single resistor could suffice. This occurs for 14a - 14d, 16a - 16d, and 17a - 17b. The purpose of

placing identical resistors in series is to increase the voltage capability of the small, low wattage,

carbon film resistors used. Individually, these resistors are only rated at from 300 to 500 volts

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(RMS). By creating resistor groups in series, the voltage rating of each group is increased

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proportionately to the number of resistors used. For example, if the peak voltage out of diode 13e can exceed 3000 volts and the combined clamping voltage of the zener diodes 42a is 2000 volts, using the resistors in series is appropriate. These implementation details are necessary for the circuit to operate within the prescribed tolerances, but the specific component values

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As mentioned, a drawback of using electrostatic speakers which require a bias on the

diaphragm is that the bias charge must first build up before the electrostatic speaker can operate.

described are not necessary for the simplified embodiments of the invention to work.

If the program signal is sent to the electrostatic speaker before the speaker is charged, then the

program will not be heard at its proper volume. It is advantageous to "pre-charge" a signal bias

supply so that it is already at an optimum voltage before the program material to be reproduced is

supplied to the electrostatic loudspeaker. The present invention provides a more effective startup

for the electrostatic speakers by using greater multiplication stages in the voltage multiplier

circuit. The bias supply also uses a separate charging signal delivered from the associated active

electronics to provide a charge on startup. Of course, the separate charging signal could also

charge periodically or on a steady basis. If the pre-charge signal is sent periodically, this helps

charge the diaphragm when it is idle for a period of time. The diaphragm might be idle between

program segments, while the program signal has been turned off and the system remains on, or

during a period of quiet in the program signal. For example, pre-recorded music will normally

have several seconds of quiet between each selection which may allow the diaphragm voltage to

fall. Similarly, most music players have a pause button which can pause the music and may

allow the diaphragm to discharge.

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Alternatively, the charging signal can be applied when the voltage on the diaphragm falls

below a pre-determined level. An additional feedback circuit is required in this configuration to

test the voltage level of the diaphragm and to determine when the charging signal should be sent.

Typically the voltage level only falls below a pre-determined level when no signal is present but

it is possible that the diaphragm voltage could decrease if the signal was very low or relatively

weak.

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The pre-charge signal can be derived from the associated active electronics, such as a

power amplifier or pre-amplifier electronics. A pre-charge signal can be audible such as that

generated from the turn-on thump of a power amplifier or it can be inaudibly derived from a

signal that operates outside of the audible range of the electrostatic speaker, such as an ultrasonic

or subsonic signal.

An ultrasonic charging signal can be generated from a simple sinusoidal oscillator,

operating in the 25 to 30KHz frequency range. This signal could even be input into the main

amplifier whose output is already coupled into the speaker matching transformer. This is

particularly suitable for a startup charge.

In some cases, a separate amplifier oscillator may be used to generate the ultrasonic

signal and provide an isolated power source in series with the main amplifier output to the step-

up transformer. Alternatively, a subsonic signal can be generated and used to bias the

diaphragm. The use of a subsonic signal is defined as a signal of low enough frequency that the

electrostatic speakers will not reproduce it or the signal is below human audibility. Using a

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subsonic signal is desirable because it is a charging signal which cannot be heard by humans and

it avoids the thump associated with amplifier power up.

In most cases, (such as using a sub-harmonic charging frequency) it would be preferable

to use the main amplifier to boost the signal to the speaker matching transformer, and to the level

needed to develop the operating bias for the electrostatic speakers.

A pre-charging signal can also be used with a parametric loudspeaker which uses an

electrostatic transducer. In this configuration, the ultrasonic charging signal source can be a

signal from the modulator electronics. This type of charging signal may also be used with the

self bias supply of the current invention and the transducer for the parametric loudspeaker.

FIG. 7 illustrates a block diagram of the invention when used as part of a parametric

loudspeaker system. The parametric modulator 70 produces a constant carrier frequency output,

usually in the range of 30 kHz to 60 kHz which is well above the range of human hearing. This

constant carrier output is independent of the program material being played through the system.

As the carrier output flows through the power amplifier 72 and transformer 10 to the self bias

circuit 74, the bias supply is charged prior to the delivery of program material such that the

parametric transducer 76 is pre-biased for operation and optimized to play program material

when the program signal is actually applied.

Referring now to FIG. 8, another embodiment of this invention uses an electrostatic

speaker system with two or more transformers. In this configuration, each speaker has its own

power transformer to power the stators. A separate self bias for the speaker diaphragm is then

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center tapped off of the transformer. Each speaker may be connected to a separate program

signal or it may only carry the high and low frequencies for a certain signal.

Despite the straight forward configuration described, using a transformer for each speaker

presents some problems. The major problem is that each speaker will have a different actual

voltage bias on the speaker diaphragm. This bias difference is due to variations in materials and

construction. So when the program signal is reproduced, one of the speakers may have a higher

volume than the other or the stereo effects may be distorted as a result of the different diaphragm

voltages.

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The preferred embodiment of self biasing using more than one transformer is to bias all

the diaphragms from a common voltage source. FIG. 8 shows a pair of stators, 90 and 92, for the

first electrostatic speaker. A second set of stators for the second speaker are shown as 94 and 96.

Each of the transformers 98 and 100, receive AC inputs to a primary winding, and the secondary

windings create a stepped up voltage for the electrostatic speakers. It is important to note that

each stator 90, 92, 94, and 96 is powered from transformer taps 102, 104, 106, and 108

respectively. Each of the diaphragms is connected to a single rectifier and voltage regulator 112

which is connected to the center taps 110a and 110b from both of the transformers 98 and 100.

This may not be practical or cost effective in some systems from a spatial point of view, if the

speakers are physically distant. Nevertheless, it is preferable to bias all the speaker diaphragms

in a multiple speaker system from the same regulated voltage supply.

FIG. 9 shows a schematic of a self bias supply where the zener diodes are located near the

secondary winding taps. Two stators 124 and 126 are powered from the high voltage taps 138

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and 140 of the secondary winding. The center tap or bias return 120 is connected to two speaker

membranes 129 and 130 and includes a capacitor 132 to aid in voltage regulation. Two zener

diodes 134 and 136 are electrically located near the high voltage bias taps 138 and 140, and limit

the voltage from the secondary windings of the transformer. It should be realized that although

only two zener diodes are shown, each diode actually represents approximately 10 or more 200

volt diodes which regulate the 2000 - 3000 volt output of the step up transformer 122.

FIG. 10 shows a self bias supply with the bias connected to a single stator 150 and the

high voltage signal connected to two separate diaphragms 152 and 154. The electrical

components of this schematic diagram are explained in further detail in FIG. 4A above. The

physical construction of the speaker shown in the schematic diagram of FIG. 10 is a single stator

with a diaphragm on either side of the stator. This physical arrangement is shown and described

in patent applications Serial No. 09/207,314 by Croft, et al and Serial No. 09/375,145 by Croft,

et al. which are herein incorporated by reference.

FIG. 11 shows the bias return tap 162 (or center tap) and one tap from the high voltage

signal winding 164 coupled to the diaphragm 160. Another tap from the high voltage secondary

winding 166 is connected to the stator 168. This arrangement drives a single stator 168 and

single self biased diaphragm 160. It should also be apparent from this disclosure that the stator

and diaphragm in FIG. 11 could be switched.

It is to be understood that the above-described arrangements are only illustrative of

certain embodiments of the present invention. Numerous modifications and alternative

arrangements may be devised by those skilled in the art without departing from the spirit and

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scope of the present invention. The appended claims are intended to cover such modifications and arrangements.